Polyvinylcarbazole Foams. I. Preparation

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Synopsis

The polymerization of vinylcarbazole in aqueous dispersion by azobisisobutyronitrile can yield—depending on the protective colloid used—polyvinylcarbazole beads or granules. These require impregnation by a polymer solvent and preferably also by azobisisobutyronitrile before they can be molded to panels or simple shapes.

INTRODUCTION

Polyvinylcarbazole has since its first discovery evoked interest, especially owing to its good dielectric properties at radar frequencies and a softening range above those of polystyrene, polyethylene, and even polyurethanes.^{1,2} The bulk polymer is very hard and rather brittle. It has been commercially available as a molding powder made by polymerization of vinylcarbazole in hot aqueous dispersion initiated by alkaline dichromate^{3,4} and marketed in Germany as Luvican M-150 and in U.S.A. as Polectron.

Polymerization in aqueous dispersion⁵ with the use of a free-radical initiator system of di-*tert*-butyl peroxide and azobisisobutyronitrile^{6,7} has yielded porous polymer beads or granules, which could be molded under light pressure to simple shapes of densities down to 0.1–0.2 g./cc. At 20°C. the dielectric constant of polyvinylcarbazole in such moldings ranged between 2.92 and 3.15, both at 1 and 44 Mcycle/sec., while the power factors under the same conditions were in the range $8-16 \times 10^{-4.5}$

The preparation of foamed polyvinylcarbazole by molding a mixture of polyvinylcarbazole powder and trihydrazinotriazine has been claimed.⁸ Several patents describe the making of polystyrene and of styrene-vinylcarbazole copolymer foams, by dispersion of the polymer powder in a solvent-nonsolvent mixture, followed by heating of the impregnated polymer.⁹⁻¹¹ In another process,¹² which might appear more appropriate to polyvinylcarbazole, the polymer is dissolved in a low-boiling solvent (methylene dichloride), the solution is dispersed in water, and most of the solvent is removed by nitrogen spraying. The resultant granules are partly dried and molded hot with appreciable expansion, densities down to 0.03 g./cc. being claimed. A method for obtaining reticulated porous polymers from several vinyl polymers, including poly(vinyl chloride), involves the impregnation of the bulk polymer with a plasticizer followed by its removal.¹³

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The present work is limited to the polymerization of vinylcarbazole to foamed beads and granules and the molding of these in the density range 0.04-0.2 g./cc.

Vinylation of carbazole is at present the only important source of the monomer. Impurities in the latter are mainly introduced with the carbazole, and of these sulfur compounds⁵ and anthracene¹⁴ are known to have a deleterious effect upon its free radical-initiated polymerization. Fortunately monomer available from B.A.S.F. Chemicals Ltd. proved sufficiently free from sulfur-containing impurities, and the best quality material (twicerecrystallized grade, unfortunately no longer available) contained too little anthracene to affect the aqueous dispersion polymerization. However, the once-recrystallized grade monomer was found to contain enough anthracene to exert a harmful effect¹⁴ and to require purification of the monomer.

Bulk polyvinylcarbazole of improved appearance and of higher molecular weight is obtained with the use of azobisisobutyronitrile as sole initiator^{14,15} rather than together with di-*tert*-butyl peroxide.⁵⁻⁷ In aqueous dispersion di-*tert*-butyl peroxide has now been found not to affect the polymerization initiated by azobisisobutyronitrile.

The size of the expanded polymer granules depends on the conditions of polymerization. Very small granules do not expand on molding. Granules of 0.5-1.5 mm. in diameter, described hereafter as beads, and larger granules of 0.5-5 mm. diameter, described hereafter as granules, expand on molding.

The aqueous dispersion polymerization requires quite careful control of conditions if a reproducible and satisfactory product is to be obtained; conditions for the polymerization of up to 2 kg./batch were established.

The polymer granules and beads from which acetone-soluble impurities and most volatiles have been removed expand on heating above 170°C., but when molding to a density below 0.2 g./cc. was attempted, intergranular cohesion upon molding was found to be very poor. Impregnation of the granules with dioxane or benzene and with azobisisobutyronitrile¹⁶ resulted in much-improved molding properties and panels up to $6 \times 6 \times 2$ in. or $12 \times 12 \times 1$ in. were molded satisfactorily from polymer granules down to a density of 0.05 g./cc. It was hoped that moldings of a more uniform porous structure could be obtained from polymer beads, and conditions for molding these into panels ($6 \times 6 \times 1$ in.) at a density of 0.1 g./cc. were established.

The molding of a simple shaped structure from impregnated granules was attempted successfully.

MATERIALS

N-Vinylcarbazole (B.A.S.F. Chemicals Ltd.) was the once-recrystallized grade. A superior (twice-recrystallized) grade monomer suitable for the dispersion polymerization without further purification was available only during the earlier part of the work.

Azobisisobutyronitrile (AIBN) was Genitron (Whiffen & Sons Ltd.), L.M. grade. This was the only one of several grades satisfactory for the polymerization, and was used also for impregnation.

Di-tert-butyl peroxide was obtained from Laporte Chemicals Ltd.

Poly(vinyl alcohol) was Elvanol (Du Pont Ltd.), grades 52:22 and 51:05. Polyvinylpyrrolidone was from B.O.C. Ltd.

Poly(ethylene glycol)-1000 monooleate, Nonex 64 (Union Carbide Ltd.), The results from several samples showed this to be the best prowas used. tective colloid for aqueous dispersion polymerization to polyvinylcarbazole granules, but with more recent samples persistently bad results were ob-This reagent was apparently made by half esterification of polytained. (ethylene glycol) of average molecular weight 1000, but of undefined molecular weight distribution. For satisfactory results a narrow cut poly-(ethylene glycol) seems necessary. Other poly(ethylene glycols) used were poly(ethylene glycol)-200 monolaurate, Nonex 31; poly(ethylene glycol)-200 monostearate, Nonex 54; poly(ethylene glycol)-400 mono laurate, refined, Nonex 139; poly(ethylene glycol)-600 monooleate, Nonex 52; poly(ethylene glycol)-1000 monolaurate, Nonex 94; and a mixed poly-(ethylene glycol)monooleate, Nonex 33, consisting of equal parts of the monooleates of poly(ethylene glycol)-300 and poly(ethylene glycol)-1540. The numbers in each case refer to the aggregate molecular weights of the poly(ethylene glycols) (all Union Carbide Ltd.).

Porofor BSH (75% benzene sulfohydrazide, 25% paraffin oil), Porofor TR (substituted thiotriazole), Porofor D33 powder (diphenylsulfone disulfohydrazide), Porofor B13/CP 50 (50% benzene disulfohydrazide, 50% chlorinated paraffin), and Porofor S44 (a disulfohydrazide) were all Bayer A.G. products, obtained through K.M. Steel, Manchester.¹⁷

Dioxane was from Griffin & George Ltd., technical and analar grades.

Methylene dichloride, chloroform, carbon tetrachloride (B.D.H. Ltd. and Griffin & George Ltd.) were laboratory grade.

B.S. Plasticiser (n-butyl cyclohexyl phthalate) was from Howard's of Ilford.

Silicone stop-cock grease was from Edwards High Vacuum Ltd.

Oxygen and nitrogen were White Spot grade; argon was from British Oxygen Co. Ltd.

EQUIPMENT

Dispersion polymerizations up to a batch scale of 800 g. monomer were carried out in mold-blown, dome-shaped Pyrex vessels (A.D. Wood, Ltd.), (5 in. deep, 5 in. i.d., 750 ml. capacity; 7 in. deep, 6 in. i.d., 2 l. capacity; or $9^{1/2}$ in. deep, 7 in. i.d., 3.2 l. capacity). These were closed by a stainless steel top plate, fitted with a nylon-packed stirrer gland, a charging port, and openings for a thermometer and a condenser, and provided with suitable positioned holes for fixing to a stirrer frame. The top plate was fitted to the glass vessel by a rod frame of suitable size and was held in position by bolts. Agitation and heating were provided by stirrers sited in a bank equipped to hold three vessels in a water bath fitted with an immersion heater. The bank was fitted with a constant speed motor ($^{1}/_{8}$ h.p., 1440 rpm) and a variable speed gear drive, allowing stirrer speeds of 200–1100 rpm.

For polymerization of 800–1800 g. monomer a 10-l. bolt head flask or a 20-l. polypropylene vessel was used; these were heated and stirred in a separate rig designed to hold only one of these.

The wing stirrer developed for the 200-g. scale was made from 17 gauge stainless steel plate, 6–7 mm. wide, of a diameter of 12.5 cm. and a height of 6.0 cm., and was found to be satisfactory up to a batch scale of 1.8 kg.

Molded foamed polymer panels were made in a simple press built round two brass ($^{1}/_{2}$ in. thick) platens of about 13 \times 14 in. Each of these was fitted with an electric heater element rated at 6 kw. and controlled by a thermostat (Diamond H, Electricity Board), the temperature being sensed by chromel-alumel thermocouples inserted into the platens. Compensation for convection losses was provided by insulating material placed around the molding frame.

The molding frames for $6 \times 6 \times 1$ in. and $12 \times 12 \times 1$ in. moldings consisted of top and bottom plates of 1/4 in. mild steel. For the $12 \times 12 \times 1$ in. frame these plates were 14×15 in. An outer frame $(13 \times 13 \times 1 \text{ in.}$ i.d.) was soldered on and an inner frame $(12 \times 12 \times 1 \text{ in. i.d.})$ was serewed to the lower plate. The 3/8 in. gap between the two frames provided air insulation or could be filled with asbestos, and it was fitted with two thermocouple pockets. The top plate was hinged to the bottom plate, and was locked on the opposite side to the outer frame by a bolt and hole fitment.

Shaped moldings in the shape of a flanged hemisphere of an outer diameter about 18 cm. and a thickness about 1/2 in. (volume 813 ml.) were made in a two-piece steel mold, the molding surfaces being of polished stainless steel. The top of the mold was held to the body by simple quick-closing clamps. Sixteen 1/16 in. vertical holes were drilled equidistantly through the upper outside edge of the top plate to allow venting of vapors during molding. This mold was heated in an air oven.

EXPERIMENTAL

Relative viscosities were determined on a 1% benzene solution of the polymer at 20°C. in an Ostwald viscometer, type A, for relative viscosities below 2.5 and in a type B instrument for relative viscosities above 2.5.

Anthracene determinations were by polarography following the procedure of Given and Peover¹⁸ with the use of tetrabutylammonium iodide in dimethylformamide.¹⁴

For aqueous dispersion polymerization to beads, monomer (500 g., oncerecrystallized grade, recrystallized once from methanol), distilled water (1750 ml.), and Elvanol (5 ml. of 3% aqueous solution) were charged to the reactor bowl heated in a water bath (90°C.). Stirring (700 rpm) was started when the monomer had melted, and upon the reactor temperature rising to 90° C. a solution of AIBN (0.5 g.) in acetone (3 ml.) was added. The polymerization became exothermic 3–8 min. after catalyst addition. After a further 10 min. stirring was discontinued, and the beads were filtered, washed with distilled water, and dried at 80° C. The beads were extracted with methanol at ambient temperature and with boiling acetone, and were air dried.

For aqueous dispersion polymerization to granules, monomer (200 g., twice-recrystallized grade or once-recrystallized grade, recrystallized again from methanol), distilled water (700 ml.), and Nonex 64 (3% aqueous solution, 10 ml.) were charged to the reactor and were heated in the water bath with stirring at 700 rpm until the reactor temperature had reached 70°C., when AIBN (4 g.) dispersed in a little acetone was added. After 4–10 min. the temperature rose sharply, and 15 min. later stirring was discontinued, and the polymer granules were washed with distilled water and dried at 80°C.

Di-*tert*-butyl peroxide (0.4 g.), when used, was added before the addition of AIBN at a reactor temperature of 65°C. The granules were extracted with methanol at ambient temperature and with boiling acetone and were air dried.

For the impregnation of polymer granules these (1 kg.) were covered with a solution of AIBN (60 g.) in dioxane (500 ml.) and acetone (1500 ml.). After standing overnight at ambient temperature the granules were drained, spread on cardboard trays to a depth of less than 1 in., and dried at 60– 80°C. During the first stage of drying, they were raked every 2–3 min. to avoid cohesion. Drying was continued until the weight of the granules corresponded to the correct weight increase. The granules were stored in well-stoppered bottles.

To mold a $12 \times 12 \times 1$ in. panel of density 0.1 g./cc. granules (260 g.) were impregnated as above and dried to a weight increase of 6.7%. They were charged quickly and evenly to the preheated (250°C.) molding frame, whose inner surfaces had been greased very lightly (one application sufficing for several moldings) with silicone stopcock grease. The frame was closed quickly and heated in the molding press in the temperature range 230–250°C. for a period of 6 min., vapors being vented every 2 min. Finally the frame was immersed in distilled water for 1 min. and the molding was dried to constant weight at 80°C. The remaining volatiles could be removed by heating at 130°C. and at 160°C. for 24 hr. each.

RESULTS

Purification of Vinylcarbazole

The twice-recrystallized grade monomer was colorless and contained less sulfur (10-22 ppm sulfur by chemical analysis, 5-15 ppm sulfur by radioactivation analysis) than seemed likely to affect its polymerization by AIBN, and no detectable anthracene (<60 ppm).¹⁴ The once-recrystallized grade vinylcarbazole had a very light yellow hue and a characteristic

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odor not noted with the better grade material. Its sulfur content was 23–25 ppm (by chemical analysis), but the concentration of anthracene (about 400 ppm) was sufficient to slow down the rate of bulk polymerization by AIBN and to lower the molecular weight of bulk polymer made from it.

The twice-recrystallized grade monomer could be polymerized satisfactorily in aqueous dispersion to either beads or granules, but these were obtained with difficulty from the once-recrystallized grade monomer, and when obtained were of lower molecular weight. It was therefore necessary to purify this monomer. Recrystallization from methanol was found to be satisfactory, anthracene being removed sufficiently by one recrystallization, provided conditions were such as to avoid the separation of molten monomer (vinylcarbazole, m.p. 64.75°C., solubility in methanol at boiling point 307 g./kg.; methanol, b.p. 64.65°C.; molar elevation of boiling point of methanol, 0.83°C./kg.). Upon separation of molten monomer from the solution the anthracene partitions between the two phases, and its separation from the monomer is much less effective. During the recrystallization, trace acid contamination and prolonged boiling had to be avoided, since vinylcarbazole adds methanol under these conditions to yield 9-(1'-methoxyethyl)carbazole,¹⁹ which is very soluble in methanol. While it did not affect the polymerization,¹⁴ its formation resulted in the loss of monomer.

The recrystallization did not require an inert atmosphere.

Use of one of a number of adsorbents during the recrystallization was not found advantageous.

Dispersion Polymerization to Beads

Foamed polyvinylcarbazole beads (0.5–1 mm. diameter) suitable for molding were made by aqueous dispersion polymerization with the use of poly(vinyl alcohol) as protective colloid and AIBN as initiator (Table I). The concentration of the protective colloid depended on the quality of the

	Aqueous I	Dispersion I	Polymerizati	on of Ving	ylcarbazole t	o Foamed Beads
Mono-	Elvanol	Wt	Temp.	Conver-	Poly	vinylcarbazole
(500 g.) ^a	soln., ml.	AIBN, g.	addition, °C.	sion, %	Relative viscosity	Appearance
Α	1.2	10	70	90	_	Fine beads
Α	2.5	10	70	89	—	Fine beads
Α	3	0.5	80		3.65	Small beads
Α	3	0.5	85		4.03	Beads, 1.0–1.5 mm.
Α	3	0.5	90		5.0	Lump
Α	6	0.5	87	—	5.5	Beads, 0.5–1 mm.
в	3	0.5	80		2.22	Beads
в	5	1.0	85		2.99	Beads
в	5	0.5	90		2.95	Beads

TABLE I

* Monomer code: A =once-recrystallized grade, recrystallized once from methanol; B =once-recrystallized grade, as received.

monomer, more being required with the once-recrystallized grade than with the twice-recrystallized grade. The twice-recrystallized grade monomer resulted in polymer of higher molecular weight than could be obtained from the once-recrystallized grade monomer.

Dispersion Polymerization to Granules

The reported polymerization to foamed granules (2–5 mm.)⁵ could not be reproduced with Elvanol as protective colloid; polyvinylpyrrolidone (relative viscosity 1.26–1.33) also proved unsatisfactory.

Certain of the half esters of poly(ethylene glycol) of the Nonex range gave better results, the best being obtained with Nonex 64 (Table II). Under optimum conditions Nonex 52 and Nonex 99 might also be suitable.

The conversions to granules in presence of Nonex 64 were notably higher than those quoted for Elvanol;⁵ the molecular weights were, however, somewhat lower than those obtained with Elvanol, both in the earlier⁵ and present work.

While seeking a satisfactory protective colloid, several stirrer types were examined and the optimum speed ranges of the best of these were shown to be in the range 500–900 rpm (Table III).

Nonex 64 with the best stirrer type at the optimum speed provided satisfactory dispersion up to a batch scale of 1.8 kg. monomer.

To assess the quality of the polymer produced, its expansion and cohesion on heating were tested, and, wherever possible, a small disk (2 in. diameter, 1 in. thickness) was molded.

Granules could not satisfactorily be obtained from the once-recrystallized grade monomer under the conditions suitable for the higher grade material. Under the microscope both grades of monomer appear similar, consisting of discrete crystals about 0.5 mm. long and weighing 1–2 mg. On dispersing the monomer in hot water containing Nonex 64 under polymerization conditions, but in absence of any initiator, and then cooling, the twice-recrystallized grade monomer was recovered in essentially spherical granules 1–2 mm. in diameter and weighing 10–20 mg., while the once-recrystallized grade monomer was isolated in small discrete crystals similar to those of the original monomer.

Polymer granules might thus be obtainable from once-recrystallized grade monomer by reducing the Nonex 64 concentration. This was found to be the case, but even under the best conditions the molecular weight of the polymer was found to be appreciably lower than that from the higher grade monomer.

The aqueous dispersion polymerizations were carried out under air. Alteration of the oxygen concentration affected the time interval between the addition of the initiator and the point at which the polymerization became exothermic (Table IV). Under nitrogen and argon the polymerization proceeded faster and yielded polyvinylcarbazole which was only partially soluble in benzene; the benzene-soluble fraction had a somewhat higher molecular weight than polymer prepared under air.

No	nex	St	irrer			Polymer			
Туре	Vol., ml.	Туреь	Speed, rpm	Conv., %	Rel. visc.	Appearance	Expan- sion•	Cohe- sion ^d	Disk•
64	0.5	Α	600	94.7	2.07	Light, rocklike mass	+	++	+
64	1	Α	600	96.5	2.07	Light, rocklike mass	+	++	+
64	5	Α	600	98.5	1.77	Large, regular, rough granules	++	++	+++
64	10	А	600	88	3.17	Large, regular, rough granules	++	++	++
64	10	В	1380	82	2.65	Large, regular, rough granules	++	-	-
64	5	С	600	86	2.80	Large, uniform granules	++	+	_
64	5	D	600	87.3	2.66	Large, uniform granules	++	++	-
31	10	С	600	87.6	2.65	Large, expanded mass	+/++	÷	+
31	10	С	600	83.7	2.65	Large, expanded mass	+/++		-
52	10	\mathbf{C}	600	88.2	2.30	Small lumps	++	++	+
99	10	В	1380	80	2.95	Irregular large granules and fines	++	-	_
139	10	С	600	85.4	2.65	Large expanded mass, lighter than water	+	+	+

			\mathbf{T}	ABLE II					
Aqueous	Dispersion	Polymerization	of	Vinylcarbazole	in	Presence	of	Nonex	Range
		Pro	tec	tive Colloids ^a					

^a Materials: half the quantities given under Experimental for polymerization to granules were used (including di-*tert*-butyl peroxide).

^b Stirrers: (A) glass link, diameter 9 cm.; (B) six-bladed stainless steel impeller, diameter 5.6 cm.; (C) stainless steel wing stirrer, diameter 7.7 cm.; (D) stainless steel two-bladed stirrer, diameter 7.0 cm.

• Code: ++++, mold forced open; +++, mold filled; ++, moderate, some cavities; +, slight expansion; -, no expansion.

^d Code: +++, granules completely fused, boundaries merged; ++, moderate, granules fused, boundaries clearly visible; +, granules badly fused and easily broken; -, no fusion.

 $^{\circ}$ Code: +++, smooth surfaces, well-formed edges; ++, fairly good surfaces, irregular edges; +, disk incompletely formed; --, no disk formed.

The elementary composition of the polymer was not affected markedly by the atmosphere under which it was polymerized.

The structure of the polymer granules was that of a labyrinth of spaces of various sizes and shapes surrounded by a hard outer shell of polymer. The microscopic structure of the outer shell could vary widely ranging from very irregular, rough and porous to very smooth.

In attempts to determine the nature of the gas in the granules, freshly made granules were washed with water, methanol, and acetone, and were

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Aqueous Dispersion of Polymerization of Vinylcarbazole: Effect of Stirrer Type and Speed^a

Sti	irrer	Tip veloc-	Polv-			Polymer		
	Speed,	ity,	meriza-	Conv.,	Rel.		Expan-	Cohe-
Туре	rpm f	t./min.	tion rat	e %	visc.	Appearance	sion	sion
С	300	240	Very rapid	93.3 I	2.07	Expanded to fill reactor, friable porous sponge	+	++
D	300	220	Very rapid	97.3 l	2.12	Expanded to fill reactor	+	++
С	400	320	Rapid	90.7	3.07	Two large pieces and some elongated granules	+	+
D	400	290	Very rapid	91.6 I	3.32	Solid mass, $d < 1$ g./cc.	+	+
С	500	400	Fairly	- 	2.70	Granules of fairly uniform size, $d < 1$ g./cc.	++	—
D	500	370	Fairly	- 	3.32	Small and moderately sized irregular particles	÷	+
С	600	480	Fairly	86.0	2.80	Large, uniform granules	++	+
D	600	44 0	Fairly	- 87.3 I	2.66	Large, uniform granules	++	++
\mathbf{C}	700	560	Slow	86.8	2.86	Uniform granules	++	
D	700	510	Slow	88.4	2.99	Uniform granules	++	+
\mathbf{C}	800	640	Fast	80.3	2.66	Expanded mass, $d < 1$ g./cc.	+	+
D	800	590	Slow	82.7	2.86	Fairly small granules	_	
С	900	720	Fast	85.4	2.48	Smooth granules, $d < 1$ g./cc.	+	-
D	900	600	Mod- erate	91.0 ,	2.84	Smooth granules, $d < 1$ g./cc.	++	++

^a Materials: Nonex 64; otherwise materials, conditions, and codes as for Table II.

TABLE IV
Aqueous Dispersion and Polymerization of Vinylcarbazole
Under Various Gas Atmospheres ^a

	Time from AIBN addn. to start		Poly	mer
Atmosphere	of temp. rise, min.	Conversion, %	Rel. visc. ^b	Appearance
Argon	2	75.3	(3.16)	Lump
Nitrogen	2.5	72.5	(3.32)	Lump
Air	7-8	88	2.60	Granules
Air	7–8	92	2.60	Granules
Oxygen	30	70	1.52	Yellow, tacky lump
Oxygen	20	88.5	1.65	Slightly cohering granules

^a Materials and conditions as given under Experimental.

^b Relative viscosities in parentheses refer to the benzene-soluble fraction of particleinsoluble polymer.

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then kept under water until ready for weighing. After weighing, the granules were immediately dissolved in hot benzene, and the separating gas was analyzed in an Atlas mass spectrometer. Analysis of the gas (4.65 ml. at NTP) from such granules (2.69 g.) showed it to consist of N₂, 77.9%; O₂, 20.8%; A, 0.7%; CO₂, 0.6 vol.-%, indicating that very soon after their preparation the granules are filled with air. Attempts at further elucidation by polymerization under argon yielded foamed polymer lumps (Table IV), which proved unsuitable sources of gas samples.

The density of polymer granules as formed in the polymerization was usually, but not invariably, below 1.0. Until dried the granules always contained water. The ease with which they were dried points to the porosity of their surface.

Purification of Polymer Granules and Beads

The dried foamed polymer granules or beads were extracted with methanol at ambient temperature and with boiling acetone. Adequate extraction particularly of beads was essential for satisfactory molding properties. The extracted granules or beads were air dried.

The acetone extract (3-6%) on unextracted polymer) consisted largely of monomer and of polymer of low molecular weight (relative viscosity 1.28) probably largely formed from the residual monomer during the extraction. A novel decomposition product of azobisisobutyronitrile, m.p. 104–106°C. (found, C, 62.1%; H, 9.2%; N, 18.2%; C₈N₁₄N₂O requires C, 62.3%; H, 9.2%; N, 18.2%) was also isolated. Its infrared spectrum indicates the presence of a nitrile and of a noncyclic secondary (probably isopropyl) amide group, and is consistent with the structure (CH₃)₂C(CN)NHCOCH-(CH₃)₂.

The relative viscosities quoted for granules and beads were determined following the preceding extraction and drying. The size distribution (by sieving) of the granules (>1/4 in., 8-17%; 1/4-3/16 in., 39-49%; 3/16-1/8 in., 30-47%; 1/8-1/32 in., 4-6%) and their bulk density (0.36-0.48 g./cc.) were also determined at this stage.

Impregnation and Molding of Polymer Granules

While the foamed, methanol- and acetone-extracted polyvinylcarbazole granules generally expanded readily on heating above 150° C., cohesion between the expanding granules was insufficient to give the molding (especially at densities <0.1 g./cc.) appreciable mechanical strength. This was considered to be due either to protective colloid in the granule surface exerting a repellant effect, or to some intrinsic property of the polymer.

Very thorough hot extraction of polymer granules (relative viscosity 2.12) with acetone and/or methanol and/or water followed by drying resulted in deterioration of cohesion upon molding at 250°C.

Attempts to mold at 250°C. ground, water- and methanol-washed polymer granules (in which the original granule surfaces had been destroyed)

	Ð	fect of S	Solvent	Impreg	nation U	T pon the	ABLE V Molding I	ropertie	s of Polyviny	lcarbazole C	iranules*
Impre	gnation			f		Mold	ding condit	ions			
	Vol.	Ace-	Poly-	Dry	Ing	Poly-		!			Moldine
	solvent,	tone,	mer,	Temp.,	Time,	mer,	Temp.,	Time,			MUIUIU
Solvent	ml.	ml.	ங்	°.	min.	Sio	°C.	min.	Expansion ^b	Cohesion ^b	Appearance
None	1	ļ	I	1	-	7.5	250	10	l	I	No disk; discolored
C ₆ H ₆	10	190	25	70	l	7.5	250	5 L	+ + +	+ + +	Very good, no cavities
						5.0	250	5	++	+	Incompletely filled mold
C ₆ H ₆	100	100	25	70	180	7.5	250	ŝ	+ + +	+ + +	Very good, hard, fibrous
						5.0	250	က	+ +	++ ++ ++	Good, fibrous, cavities
C ₆ H ₅ CH ₃	10	190	25	100	180	7.5	250	5 2	+ +	1	Poor, slight cohesion
$C_6H_4(CH_3)_2$	10	190	25	128	180	7.5	250	ų	+	l	No disk obtained
$(CH_2)_5CO$	50	150	50	60	180	7.5	250	ŝ	+]	No disk obtained
$O(C_2H_4)_2O(C_2H_4)O(C_4)O(C_4H_4)O(C_4H_4)O(C_4H_4)O(C_4H_4)O(C_4H_4)O(C_4H_4)O($	50	150	50	80	120	2.1	218 - 224	9		ĺ	Good disk
$(CH_2)_4O$	10	190	25	70	120	7.5	250	5	+	I	No disk obtained
HCON(CH ₃) ₂	50	150	50	80	120	2.1		9]		No disk obtained
CH2Cl2	50	150	50	80	120	2.1	223 - 228	9	l		Poor disk, incompletely expanded
CHC1 ₃	50	150	50	80	120	2.1	223 - 228	9	l	l	Poor disk, expansion and cohesion
											inadequate
C2HC13	10	190	25	70	180	7.5	250	l	++	++	Fibrous disk
C ₆ H ₅ N	50	150	50	85 - 95	120	2.1	220 - 226	9	+ +	+++++	Well-fused disk, somewhat col-
											lapsed in center
$C_5H_5N + 3\%$ AIBN	l	ļ		1]	2.1	212 - 232	4	+ +	+++++++++++++++++++++++++++++++++++++++	Well-fused disk, incompletely ex-
											panded
^a Polyvinylcarbazol	e granul	es, relat	ive vise	cosity, 2.	55. Ace	tone wa	s used as di	luent.	Moldings wer	e made in a :	21/4-in. diameter, 1-in. thick, circular

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mold. ^b See Table II.

	Various Alternative Diluents ^a
TABLE VI	ng of Solution-Impregnated Polyvinylcarbazole Granules in
	Molding

						100100				
	Impregnat	ion		Dr	ying.	impregna- tion and	Molding		ļ	
		Soln.	Polymer.	Temp	Time.	drving.	temp		Disk	Ĭ
Diluent	Solvent	ml.	50	°C.	min.	19-02-02 19-02-02-02-02-02-02-02-02-02-02-02-02-02-	°C.	$\operatorname{Expansion}^{\mathrm{b}}$	Cohesion ^b	Appearance
Acetone	Benzene	100	50	80	120	8	212 - 223	++	+++++	Fair
Acetone	Dioxane	100	50	80	120	10	218 - 222	+++	+ + +	Good
Ether	Benzene	250	100	20		7	213 - 220	+++++++++++++++++++++++++++++++++++++++	+	Poor
Ether	Benzene	250	100	80	180	2	220 - 222	++	÷	Poor
Ether	Dioxane	250	100	20	l	11	220 - 222	++	+	Poor
Ether	Dioxane	250	100	80	180	5	216 - 222	++++	+	Poor
Methanol	Benzene	100	50	80	120	Н	210 - 230	+	+	$\mathbf{P}_{\mathbf{oor}}$

and 3% AIBN and were left to stand under the mixture at atmospheric pressure for 45 min. Molding times in $2^{1}/4 \times 1/2$ in. circular frame were 6 min. ^b See Table II.

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Impre	gnation					
Ben-	Drying	Mole	ling		Disk	
zene, vol%	time, min.	Polymer, g.	Time, min.	$\operatorname{Expansion}^{\flat}$	Cohesion ^b	Appearance
5	60	7.5	5	+		_
	120	7.5	5	++	_	—
	180	7.5	3	++	++	Good, but some cavities
	180	7.5	5	++	+++	Good
	180	7.5	10	++	+	Shrunk, little cohe- sion
	180	10	3	++++	+++	Hard, fibrous
	180	10	5	++	+ + +	Hard, fibrous
20	180	5	2	+++	+++	Hard, fibrous
		7.5	2	+++	+++	Hard, fibrous
25	180	5	1	++++	++	Some cavities, in- completely fused
		5	2	+++	+++	Hard, fibrous
		5	3	++	+++	Some cavities
		7.5	3	+++	+++	Hard, fibrous
- 30	180	3.75	$1^{1}/_{2}$	++	++	Some cavities
		3.75	2	+++	┽┽┼	Hard, fibrous
		5	$1^{1/2}$	++++	+++	Hard, fibrous
		5	2	+++	+++	Hard, fibrous
		5	4	++	+	Cavities, very poor cohesion
		6.6	$1^{1/2}$	+	+	Cavities, very poor cohesion
		12	2	++	++	Incomplete fusion
		15	2	+++	++	Fair

TABLE VII

Molding of Polyvinylcarbazole Granules Impregnated with Benzene-Acetone Solution*

* Approx. 8 ml./g. impregnation solution was used. For conditions see Experimental. The impregnated granules were dried at 70 °C.; Molding temperature, 250 °C. Moldings were made in a $2^{1}/_{4}$ -in. circular, 1-in. thick mold.

^b See Table II.

revealed a lack of cohesion, and the grinding also affected expansion adversely.

The possibility of chemical change during molding affecting cohesion seemed unlikely, since neither the solubility nor the molecular weight of the granules was found to be affected by molding.

Thus the poor cohesion between granule surfaces on attempted molding appeared to be an intrinsic property of the granule surface. Fusion between the surfaces (upon molding) is due to a sufficient increase in chain mobility and a decrease in chain order near the softening range. Stretching of the polymer chains would occur during expansion of the hot granules and could enhance the orientation and chain order while decreasing the chain mobility. Interlocking between the polymer molecules is likely to be exceptionally hindered by the closely spaced, large carbazole substituents lining the molecule. A polymer solvent should increase the mobility of the polymer molecules. To avoid undue softening or tackiness of the granules, the solvent was applied in a lower boiling diluent (with which it should not form an azeotropic mixture), which was chosen so as to dissolve the solvent, but not the polymer.

The effect of impregnation of polyvinylcarbazole granules (relative viscosity 2.5–2.7) with a number of solvents and related compounds in acetone solution upon their molding properties showed benzene, dioxane and pyridine to be most promising (Tables V and VI).

The granules impregnated with a 50/50 benzene-acetone solution were very tacky and had to be separated. Granules impregnated with cyclohexanone showed neither appreciable expansion nor cohesion on molding but acquired a remarkable gloss and transparency.

Rather surprisingly methanol and diethyl ether proved greatly inferior to acetone as diluents (Table VI).

Impregnation with benzene-acetone solutions allowed the molding of satisfactory disks down to a density of about 0.1 g./cc. (Table VII). In-adequate expansion rather than poor cohesion limited molding to this density.

The effect of impregnation with blowing agents upon the molding properties was therefore examined, and AIBN was selected for study, since a very pure product is commercially available which should be without deleterious effect upon the electrical properties of the product.

The effect of AIBN impregnation upon the molding properties resembled that produced by benzene or by dioxane (Table VIII). Impregnation with an acetone solution containing both benzene and AIBN gave still further improvement, so that $12 \times 12 \times 11$ in. panels of satisfactory quality could be

Impreg	nation						
		Ace-	Moldi	ng	_	Disk	
Polyvinyl- carbazole, g.	AIBN, g.	tone, ml.	Polymer, g.	Time, min.	Expan- sion ^b	Cohesion ^b	Appearance
Control (unimpreg granules)	nated		7.5	3	+++	_	_
			5	3	+	+++	Well formed, cavities
100	6	500	7.5	3	+++	+++	Well formed, some cavi- ties
			7.5	4	+++	+++	Well formed, coherent

TABLE VIII

Effect of Impregnation by Azobisisobutyronitrile upon the Molding Properties of Polyvinylcarbazole Granules^a

• Polyvinylcarbazole, relative viscosity, 2.6. The granules were evacuated under the solution until there was essentially complete penetration.

^b See Table II.

obtained down to a density of 0.1 g./cc., and smaller moldings even below this limit (Table IX). Satisfactory results were obtained with a solution of 3% AIBN in 25% benzene-acetone and still further improvement was attained when the benzene in such mixtures was replaced by dioxane. $12 \times 12 \times 1$ in. and $6 \times 6 \times 2$ in. panels could be molded down to a density of 0.05 g./cc. following impregnation with the latter mixture (Table X). The molding of $6 \times 6 \times 2$ in. panels was found to require a longer molding period than was required for the thinner moldings, especially when molding at the higher densities. If the molding period was too short, the interiors of the moldings were incompletely fused, despite their excellent outside appearance.

Mole	ling			
Polymer	Time.		Disk	
g.	min.	Expansion ^b	Cohesion ^b	Appearance
2	3	+++	 +++	Fused, fibrous
2	3	+++	+++	Fused, fibrous
3	3	+++++	++++	Good, fused, fibrous
3	3	++++	++++	Good, fused, fibrous
4	3	+++	- <u>+</u> -+-+-	Good, fused, fibrous
5	3	++++	+++	Very good, fused, fibrous
5	3	++++	+++	Very good, fused, fibrous
7.5	4	+++	+++	Very good

TABLE IX Effect of Impregnation by AIBN–Benzene–Acetone Solution upon the Molding Proper-

ties of Polyvinylcarbazole Granules^a

^a Solutions contained 3% AIBN in 25% benzene-acetone. The impregnated granules were dried for 3 hr. at 65°C. Moldings were made in a $2^{1}/_{4}$ -in. circular, $1/_{2}$ -in. thick mold at a molding temperature of 250°C.

^b See Table II.

Quantitative control of the impregnation by AIBN-benzene-acetone depended upon infrared absorption spectrophotometry. The impregnated granules were extracted with boiling carbon tetrachloride (6 hr. in Soxhlet), and the absorptions at 1710 (acetone), 1930 (benzene), and at 2230 cm.⁻¹ (AIBN) were determined in 0.1 and 1 cm. cells, varying the path length against standards. The technique could not be adapted to control of the more important AIBN-dioxane-acetone impregnation, since there is too much overlap between the stronger absorption lines of dioxane and the other components.

Attempts to evaluate and control the impregnation by determining the weight increase following impregnation and drying of the impregnated granules proved complex, since some of the polymer dissolved in the impregnation solution rendering the data difficult to interpret. With the AIBN-dioxane-acetone solutions good results when molding to densities

		Panel	Appearance	Incompletely fused, many cav- ities	Smooth, well fused	Incompletely fused, many cav-	ities	Good, smooth, few cavities	Good, smooth, few cavities	Good, smooth, few small cav-	ities	Fairly good, somewhat uneven
n e-A cetone anules			Density, g./cc.	0.054	0.059	0.059		0.11	0.11	0.18		0.11
JBN-Dioxa carbazole Gr			Time, min.	£	9	10		×	×	11		19
Acetone or by A es of Polyvinyle			Temp., °C.	220–233	209 - 220	207 - 219		215 - 220	216 - 224	205 - 220		200-219
BN-Benzene- lding Properti	Molding		Polymer, g.	35	35	35		72	72	118		288
Impregnation by AI Upon the Mc		Frame	dimensions, in.	$6 \times 6 \times 1$	$6 \times 6 \times 1$	$6 \times 6 \times 1$		$6 \times 6 \times 1$	$6 \times 6 \times 1$	$6 \times 6 \times 1$		12 imes12 imes1
Effect of	n	ing	Time, min.	120								120
	mpregnatio	Dry	Temp., °C.	80								80
	I		Solution ^a	V								A

. ATPN DS 4 TABLE X ATDN D. Ļ,

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	80 540 6 × 6 × 2 220 185-225 40 0.176 Very good 3% AIBN in 25% benzene-acetone; solution B: 3% AIBN in 25% dioxane-acetone. 3% AIBN in 25% 0.176 Very good	expanded core	80 120 $12 \times 12 \times 12 \times 1$ 400 132-202 14 0.166 Good	80 $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Very good	incompletely	very good Good Fairly good Good Very good Good Good Good Good Good Surfaces, expanded core Very good	0.10 0.066 0.067 0.103 0.103 0.103 0.166 0.177 0.065 0.065 0.065 0.113 0.113 0.113 0.113 0.192 0.192 0.176 etone.	40 40 40 40 40 40 40	149-224 149-204 245-238 245-238 132-202 245-238 132-202 245-238 149-210 205-227 139-209 188-218 188-218 188-218 185-225 3% AIBN in 25%	250 174 174 260 260 438 80 80 80 80 80 125 140 250 250 80 140 250 80 140 80 80 80 80 80 80 80 80 80 80 80 80 80	$\begin{array}{c} 12 \times 12 \times 11 \\ 12 \times 12 \times 11 \\ 12 \times 12 \times$	120 120 120 120 540 540 540 540 540 540 540 540 540 54	L: 3% 80 80 80 80 80 80 80 80 80 80 80 80 80
80 270 $6 \times 6 \times 2$ 250 188-218 14 0.192 Good surfaces, incomp	expanded core		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	incompletely	Good surfaces,	0.192	14	188–218	250	6 imes 6 imes 2	270	80
80 270 $6 \times 6 \times 2$ 140 139-209 14 0.113 Good	80 270 $6 \times 6 \times 2$ 250 188–218 14 0.192 Good surfaces, incomple expanded core	80 270 $6 \times 6 \times 2$ 250 188–218 14 0.192 Good surfaces, incompletely	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Good	0.113	14	139-209	140	$6 \times 6 \times 2$	270	80
80 540 $6 \times 6 \times 2$ 125 205-227 12 0.10 Very good	80 270 $6 \times 6 \times 2$ 140 139-209 14 0.113 Good 80 270 $6 \times 6 \times 2$ 250 188-218 14 0.192 Good surfaces, incomple expanded core	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Very good	0.10	12	205 - 227	125	$6 \times 6 \times 2$	540	80
$$ $$ $6 \times 6 \times 2$ 80 149-210 14 0.060 Good	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		$\begin{array}{cccccccccccccccccccccccccccccccccccc$			Good	0.060	14	149-210	80	$6 \times 6 \times 2$	[[
85 120 $6 \times 6 \times 2$ 80 221–228 10 0.065 Good	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	80 $12 \times 12 \times 1$ 438 245-235 6 0.177 Good	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Good	0.065	10	221 - 228	80	$6 \times 6 \times 2$	120	85
80 $12 \times 12 \times 1$ 438 245-235 6 0.177 Good	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		80 120 $12 \times 12 \times 12 \times 1$ 400 $132-202$ 14 0.166 Good		Good	0.177	9	245 - 235	438	12 imes 12 imes 1	[80
12 × 12 × 1 260 245-238 6 0.103 Good	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	80 $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Very good			Good	0.103	9	245 - 238	260	$12 \times 12 \times 1$	Į	
80 12 × 12 × 1 174 245-238 6 0.067 Fairly good	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ 12 \times 12 \times 1$ 260 245-238 6 0.103 Good		Fairly good	0.067	9	245 - 238	174	$12 \times 12 \times 1$	1	80
12 × 12 × 1 174 149–204 8 0.066 Good	$ \begin{array}{llllllllllllllllllllllllllllllllllll$	$ \begin{array}{llllllllllllllllllllllllllllllllllll$	80 $12 \times 12 \times 1$ 174 $245-238$ 6 0.067 Fairly good $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good	80 $12 \times 12 \times 1$ 174 245-238 6 0.067 Fairly good $12 \times 12 \times 1$ 260 245-238 6 0.103 Good		Good	0.066	œ	149-204	174	12 imes 12 imes 1	1	
12 × 12 × 1 472 218-227 13 0.16 Very good	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		Very good	0.16	13	218 - 227	472	12 imes 12 imes 1		I
80 120 12 $12 \times 12 \times 1$ 471 215-225 13 0.17 Very good, uniform	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ш	Very good, unifor	0.17	13	215 - 225	471	$12 \times 12 \times 1$	120	80
80 120 12 $\times 12 \times 12 \times 1$ 288 215-227 10 0.11 Very good	30120 $12 \times 12 \times 12 \times 1$ 471 $215-225$ 13 0.17 Very good, uniform $12 \times 12 \times 1$ 174 $149-204$ 8 0.066 $Good$ 30 $12 \times 12 \times 1$ 174 $149-204$ 8 0.066 $Good$ 30 $12 \times 12 \times 1$ 174 $149-204$ 8 0.067 $Fairly good$ 30 $12 \times 12 \times 1$ 174 $245-238$ 6 0.103 $Good$ 30 $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $12 \times 12 \times 1$ 400 $132-202$ 14 0.166 $Good$ 80 $12 \times 12 \times 1$ 438 $245-235$ 6 0.177 $Good$ 80 $12 \times 12 \times 1$ 490 $132-202$ 14 0.166 $Good$ 80 $12 \times 12 \times 1$ 430 $245-235$ 6 0.177 $Good$ 80 540 $6 \times 6 \times 2$ 80 $245-235$ 10 0.065 $Good$ 80 570 $6 \times 6 \times 2$ $129-10$ 14 0.166 $Good$ 80 570 $6 \times 6 \times 2$ $129-207$ 12 0.10 $Very good$ 80 270 $6 \times 6 \times 2$ 250 $188-218$ 14 0.102 $Good$ 80 270 $6 \times 6 \times 2$ 250 $188-218$	8012012 × 12 × 1471215-225130.17Very good, uniform $$ $$ $12 \times 12 \times 1$ 472 $218-227$ 130.16Very good $$ $$ $12 \times 12 \times 1$ 174 $149-204$ 80.066Good 80 $$ $12 \times 12 \times 1$ 174 $245-238$ 6 0.067 Fairly good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Very good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Very good 80 $$ $12 \times 12 \times 1$ 400 $132-202$ 14 0.166 Good 80 $$ $12 \times 12 \times 1$ 430 $132-202$ 14 0.166 Good 80 $$ $12 \times 12 \times 1$ 430 $132-202$ 14 0.166 Good 80 $$ $6 \times 6 \times 2$ 80 $245-236$ 10 0.066 Good 80 540 6×2 $149-210$ 14 0.166 Good 80 270 $6 \times 6 \times 2$ 120 $139-209$ 14 0.102 Good 80 270 $6 \times 6 \times 2$ 250 $188-218$ 14 0.102 Good 80 270 $6 \times 6 \times 2$ 250 $188-218$ 14 <td< td=""><td>80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform $$ $$ $12 \times 12 \times 1$ 472 $218-227$ 13 0.16 Very good $$ $$ $12 \times 12 \times 1$ 174 $149-204$ 8 0.066 Good 80 $$ $12 \times 12 \times 1$ 174 $245-238$ 6 0.067 Fairly good $$ $-12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Very good</td><td>80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform $$ $$ $12 \times 12 \times 1$ 472 $218-227$ 13 0.16 Very good $$ $$ $12 \times 12 \times 1$ 174 $149-204$ 8 0.066 Good 80 $$ $12 \times 12 \times 1$ 174 $245-238$ 6 0.067 Fairly good $$ $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good</td><td></td><td>Very good</td><td>0.11</td><td>10</td><td>215 - 227</td><td>288</td><td>$12 \times 12 \times 1$</td><td>120</td><td>80</td></td<>	80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform $$ $$ $12 \times 12 \times 1$ 472 $218-227$ 13 0.16 Very good $$ $$ $12 \times 12 \times 1$ 174 $149-204$ 8 0.066 Good 80 $$ $12 \times 12 \times 1$ 174 $245-238$ 6 0.067 Fairly good $$ $-12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Very good	80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform $$ $$ $12 \times 12 \times 1$ 472 $218-227$ 13 0.16 Very good $$ $$ $12 \times 12 \times 1$ 174 $149-204$ 8 0.066 Good 80 $$ $12 \times 12 \times 1$ 174 $245-238$ 6 0.067 Fairly good $$ $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 Good		Very good	0.11	10	215 - 227	288	$12 \times 12 \times 1$	120	80
	30120 $12 \times 12 \times 12 \times 1$ 288 $215-227$ 10 0.11 Very good $ 12 \times 12 \times 1$ 471 $215-225$ 13 0.17 Very good $ 12 \times 12 \times 1$ 174 $149-204$ 8 0.066 $Good$ 30 $ 12 \times 12 \times 1$ 174 $149-204$ 8 0.066 $Good$ 30 $ 12 \times 12 \times 1$ 174 $245-238$ 6 0.067 $Fairly good$ 30 $ 12 \times 12 \times 1$ 174 $245-238$ 6 0.103 $Good$ 30 $ 12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $ 12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $ 12 \times 12 \times 1$ $245-238$ 6 0.103 $Good$ 80 $ 12 \times 12 \times 1$ $245-238$ 6 0.103 $Good$ 80 $ 12 \times 12 \times 1$ 490 $132-202$ 14 0.166 $Good$ 80 $ 12 \times 12 \times 1$ 438 $245-235$ 6 0.177 $Good$ 80 $ 6 \times 6 \times 2$ 80 $245-235$ 10 0.666 $Good$ 80 540 $6 \times 6 \times 2$ $149-210$ 14 0.166 $Good$ 80 570 $6 \times 6 \times 2$ 122 122 $205-227$ 12 0.10 $Very good$ 80 270 $6 \times 6 \times 2$ 250 $188-218$ <t< td=""><td>8012012 × 12 × 1288215-227100.11Very good$$$$$12 \times 12 \times 1$$471$$215-225$$13$$0.17$Very good, uniform$$$$$12 \times 12 \times 1$$471$$215-227$$13$$0.16$Very good, uniform$$$$$12 \times 12 \times 1$$174$$215-227$$13$$0.16$Very good, uniform$80$$$$12 \times 12 \times 1$$174$$245-238$$6$$0.066$$Good$$80$$$$12 \times 12 \times 1$$260$$245-238$$6$$0.103$$Good$$80$$$$12 \times 12 \times 1$$260$$245-238$$6$$0.103$$Good$$80$$$$12 \times 12 \times 1$$260$$245-238$$6$$0.103$$Good$$80$$$$12 \times 12 \times 1$$260$$245-238$$6$$0.103$$Good$$80$$$$12 \times 12 \times 1$$400$$132-202$$14$$0.166$$Good$$80$$$$12 \times 12 \times 1$$430$$132-202$$14$$0.166$$Good$$80$$$$12 \times 12 \times 1$$430$$132-202$$14$$0.166$$Good$$80$$$$12 \times 12 \times 1$$430$$132-228$$10$$0.66$$Good$$80$$540$$6 \times 6 \times 2$$149-210$$14$$0.166$$Good$$80$$570$$6 \times 6 \times 2$$140$$149-210$$14$$0.106$$Good$$80$$270$$6 \times 6$</td><td>80 120 12 × 12 × 1 288 215-227 10 0.11 Very good 80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform 12 × 12 × 1 471 215-227 13 0.17 Very good, uniform 12 × 12 × 1 174 149-204 8 0.066 Good 80 12 × 12 × 1 174 245-238 6 0.067 Fairly good 80 12 × 12 × 1 260 245-238 6 0.103 Good 80 12 × 12 × 1 260 245-238 6 0.103 Good 80 12 × 12 × 1 260 245-238 6 0.103 Good</td><td>80 120 12 × 12 × 1 288 215-227 10 0.11 Very good 80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform 12 × 12 × 1 472 218-227 13 0.16 Very good 12 × 12 × 1 174 149-204 8 0.066 Good 80 12 × 12 × 1 174 245-238 6 0.067 Fairly good 12 × 12 × 1 174 245-238 6 0.067 Fairly good 12 × 12 × 1 260 245-238 6 0.103 Good</td><td></td><td>Fairly good</td><td>0.10</td><td>10</td><td>217 - 224</td><td>288</td><td>$12 \times 12 \times 1$</td><td>120</td><td>80</td></t<>	8012012 × 12 × 1288215-227100.11Very good $$ $$ $12 \times 12 \times 1$ 471 $215-225$ 13 0.17 Very good, uniform $$ $$ $12 \times 12 \times 1$ 471 $215-227$ 13 0.16 Very good, uniform $$ $$ $12 \times 12 \times 1$ 174 $215-227$ 13 0.16 Very good, uniform 80 $$ $12 \times 12 \times 1$ 174 $245-238$ 6 0.066 $Good$ 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $$ $12 \times 12 \times 1$ 260 $245-238$ 6 0.103 $Good$ 80 $$ $12 \times 12 \times 1$ 400 $132-202$ 14 0.166 $Good$ 80 $$ $12 \times 12 \times 1$ 430 $132-202$ 14 0.166 $Good$ 80 $$ $12 \times 12 \times 1$ 430 $132-202$ 14 0.166 $Good$ 80 $$ $12 \times 12 \times 1$ 430 $132-228$ 10 0.66 $Good$ 80 540 $6 \times 6 \times 2$ $149-210$ 14 0.166 $Good$ 80 570 $6 \times 6 \times 2$ 140 $149-210$ 14 0.106 $Good$ 80 270 $6 \times 6 $	80 120 12 × 12 × 1 288 215-227 10 0.11 Very good 80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform 12 × 12 × 1 471 215-227 13 0.17 Very good, uniform 12 × 12 × 1 174 149-204 8 0.066 Good 80 12 × 12 × 1 174 245-238 6 0.067 Fairly good 80 12 × 12 × 1 260 245-238 6 0.103 Good 80 12 × 12 × 1 260 245-238 6 0.103 Good 80 12 × 12 × 1 260 245-238 6 0.103 Good	80 120 12 × 12 × 1 288 215-227 10 0.11 Very good 80 120 12 × 12 × 1 471 215-225 13 0.17 Very good, uniform 12 × 12 × 1 472 218-227 13 0.16 Very good 12 × 12 × 1 174 149-204 8 0.066 Good 80 12 × 12 × 1 174 245-238 6 0.067 Fairly good 12 × 12 × 1 174 245-238 6 0.067 Fairly good 12 × 12 × 1 260 245-238 6 0.103 Good		Fairly good	0.10	10	217 - 224	288	$12 \times 12 \times 1$	120	80

below 0.1 g./cc. were obtained following such a weight increase of 6-10%; for molding at and above 0.1 g./cc. it should preferably be 5-7%.

Attempts to mold down to a density of 0.03 g./cc. with the use of polyvinylcarbazole granules impregnated with AIBN-dioxane-acetone to a weight increase of 8-10% have given only fairly good results, the moldings being somewhat underexpanded.

Impregnations with a solution of 3% AIBN in benzene (12.5%)-dioxane (12.5%)-acetone yielded granules of molding properties intermediate between the solutions containing either benzene or dioxane.

The lack of cohesion upon molding of rough crushed foamed polyvinylcarbazole granules was also largely overcome by impregnation with AIBNbenzene-acetone solution. The molding of smaller particles seemed desirable, since the liability to failure, especially of the thinner moldings, should be lessened. Foamed polyvinylcarbazole granules (120 g.; relative viscosity, 2.55; size distribution >1/4 in., 35%; $1/4^{-3}/16$ in., 45%; $3/16^{-1}/8$ in., 18%; $1/8^{-1}/8^{-1}$ in., 2%) were crushed to pass through a $3/16^{-1}$. sieve, and fractions $3/16^{-1}/8$ in. (31 g.) and $1/8^{-1}/32$ (82 g.) were separately impregnated with AIBN-benzene-dioxane solution and dried for 2 hr. at 80°C. Impregnation appeared to improve the molding properties of the crushed granules to a molding quality similar to that shown by the correspondingly impregnated, uncrushed granules (Table XI).

Impregnation by several Porofor blowing agents, which were unfortunately available only as rather colored mixtures with diluents (hydrocarbon or chlorinated hydrocarbon) was examined (Table XII). These blowing agents decompose to give various (often sulfur-containing) products of low volatility. The Porofors were applied as 3% solutions, 25% dioxane in acetone being used as solvent. Several of these blowing agents were insuffi-

	Molding	g			
Particle size, in.	Polymer, g.	Temp., °C.	Time, min.	Thick- ness, in.	Disk Appearance
Control	2.09	218225	6	1/2	Fairly good, many cavi- ties
Control	1.05	207-228	6	1/4	Fairly good, incompletely expanded
3/16-1/8	2.09	219-222	—	1/2	Fairly good, many cavi- ties
³ / ₁₆ - ¹ / ₈	1.05	210 - 234	6	1/4	Good, few holes
$1/8^{-1}/32$	2.09	219 - 224	6	1/2	Good, small cavities
1/8-1/32	1.05	210224	6	1/4	Good expansion, fair co- hesion

TABLE XI

Effect of Impregnation with AIBN (3%)-Benzene (25%)-Acetone Solution upon the Molding Properties of Rough Crushed Foamed Polyvinylcarbazole Granules^a

• A $2^{1}/_{4}$ -in. circular molding frame was used. The density of the moldings was 0.06-0.07 g./cc. Uncrushed, impregnated granules were used in the control experiments.

	Im	pregnatio	n				
		Woight	Drwing	Wt. incr. after impregna- tion and		Mold	ing
Porofor	Time, hr.	incr., %	time, min.	drying, %	Temp., °C.	Time, min.	Panel
TR	18	79	165	8.5	219-229	4	Very good
TR	20	74	180	10	216-230	6	Good, well fused, shrunk, light brown
BSH paste	18	76	240	9	215-233	4	Very good
BSH paste	19	72	180	10	214-225	5	Very good
B13/CP50	18	66	180	10	210-230	5	Good, fairly well fused
B13/CP50	18	64	90	11.5	216–230	6	Moderate, not very well fused

TABLE XII	
Molding of Polyvinylcarbazole Granules Impregnated with Porofor Blowing Age	nts in
Dioxane-Acetone Solution ^a	

• Polyvinylcarbazole granules (100 g.; relative viscosity 2.60) were impregnated with 200 ml. solution and were dried at 80 °C. The impregnated granules (40 g.) were molded in a $6 \times 6 \times 1$ in. frame.

ciently soluble in the solvent mixture to be used. Several of the Porofors gave rather discolored but otherwise very good moldings.

Impregnation of polyvinylcarbazole granules (50 g.; relative viscosity, 2.70) with a solution of *n*-butyl cyclohexyl phthalate (10 ml.) in acetone (190 ml.) for 2 hr., followed by drying for 3 hr. at 60° C. resulted in no marked improvement of the molding quality of the granules.

Impregnation and Molding of Polymer Beads

It was hoped that the molding of foamed polyvinylcarbazole beads would yield moldings of a finer and more uniform core structure. The solventextracted and dried beads could not be molded to satisfactory panels before impregnation, cohesion being even worse than with granules, due probably to the higher molecular weight of the beads. Impregnation with benzene gave considerable improvement, but as in the case of the granules, AIBNdioxane-acetone proved superior for this purpose. It will be noted that this treatment resulted in good moldings from beads of widely varying molecular weights (Table XIII). However, unsatisfactory moldings were also obtained, and for satisfactory results improved control of the impregnation is still needed.

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Polyvinylcarbazole.	Mole	ding	
relative viscosity	Temp., °C.	Time, min.	Panel appearance
1.72	240	6.5	Very good
2.12	240	8	Good, smooth surfaces
2.58	210	20	Good
2.99	210	15	Good
3.19	200	18	Very good
5.45	245	7	Fairly good, some rough areas

TABLE XIII	
Molding of Polyvinylcarbazole Beads Impregnated with AIBN (3%)-Dioxane (25%)	6)-
Acetone Solution ^a	

^a Following 18 hr. impregnation at ambient temperature and atmospheric pressure, the beads were dried at 80 °C. to a weight increase of 10%. Panels of density \sim 0.1 g./cc. were molded in a 6 × 6 × 1 in. frame.

Hemispherical Molding

Polyvinylcarbazole granules impregnated with a solution of AIBN (3%) in dioxane (25%)-acetone were molded (Table XIV). Very satisfactory results were obtained when the open mold, preheated to 200–220°C, was charged with the granules and then closed and the clamps set, all within

Wt. increase on impreg- nation and	Polymer	Charging	Molding		Hemisphere
drying, %	wt., g.	time, sec.	temp., °C.	Density, g./cc.	Appearance
6.9	76		214-215		Dome fairly well formed, but uneven flange an- nulus
8.0	104	210	207-210		Good, dome well formed, but flange incomplete
8.0	104	120	203-215	0.124	Good, dome and flange fully formed
8.0	104	72	195–215	0.117	Good, dome and flange fully formed

TABLE XIV Hemispherical Moldings of Foamed Polyvinylcarbazole^s

^a The charging time is the interval between removal of the preheated mold from the oven and the return to it of the charged mold. Molding time, 14 minutes.

about 1 min., before being returned to the air oven. Satisfactory moldings were soon obtained, the appropriate edges of the flange being sharp or well rounded. At the end of the molding period the mold was submerged under water for 1 min.

DISCUSSION

The aqueous dispersion polymerization of vinylearbazole is clearly a complex process in which the disperse phase must be maintained under close control while the monomer polymerizes, its physical properties changing from those of a viscous liquid through those of a tacky gum to those of a hard solid, while the heat evolved is in excess of that needed to raise the temperature of the dispersion from about 70 to 100°C.

The results indicate that polymer granules are built up from monomer droplets, and that the size of these at the outset of the polymerization intermediate between that corresponding to that of the small monomer crystals and the quantity of monomer required for a single granule—has a critical effect upon the state of the polymer. The once-recrystallized grade monomer appears to contain an impurity facilitating its dispersion in hot water. Whether this is ascribable to anthracene, which is known to be responsible for retarding the polymerization in bulk and which is known' to be present in the grade monomer¹⁴ is still uncertain.

The concentration (2%) of azobisisobutyronitrile required for polymerization to granules is much greater than that (0.1%) required for polymerization to beads. A much smaller initiator concentration (0.005-0.01%)suffices for the bulk polymerization of this monomer.¹⁴ The much greater amount of initiator needed in the dispersion polymerization is thought to be due to unfavorable distribution of the initiator between monomer and aqueous phase, but the difference between the concentrations required for granules and beads suggests a more subtle factor, which may include the size of the dispersed monomer particles and the temperature at which Thus the isolation of a low molecular decomposition initiation sets in. product of azobisisobutyronitrile $(CH_3)_2C(CN)NHCOCH(CH_3)_2$ from the granular polymer indicates that even initiator dissolved in the disperse monomer does not initiate efficiently (unless this product is formed from initiator dissolved in the aqueous phase and then contaminates the wet polymer granules). Whether the lower molecular weight of the polymer made from the once-recrystallized grade monomer is solely ascribable to the presence in it of a little anthracene is also still uncertain. There is no evidence that degradation of the protective colloid by the radicals produced from the initiator occurs and is accountable for some of these complex features.

In forming expandable beads the polymerizing monomer droplets are thought to coalesce to a large degree, depending upon the protective colloid with the formation of voids in the polymerizing phase. With Elvanol (a strongly hydrophilic protective colloid), these beads remain separate during the polymerization despite their tacky surface, but with a more lyophilic protective colloid, the separate particles coalesce forming granules, lumps, or even a single piece of expanded polymer. The conditions required for granules are thus likely to be more exacting than those required for beads, and this is found to apply.

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Incorporation of the protective colloid into the granule surface either by solution or grafting does not apparently contribute to the difficulties encountered in molding granules, but may help to account for some inconsistencies applying to the molding properties of the polymer beads.

The effect of oxygen upon the dispersion polymerization is typical for The formation of some benzene-insoluble polymer free-radical reactions. when the polymerization is carried out under an inert atmosphere is particularly interesting. The insolubility in benzene of part of the polyvinylcarbazole product during the cationic polymerization^{20,21} by boron trifluoride etherate in methylene dichloride has been ascribed to crosslinking.²⁰ Insolubility in benzene of part of the polyvinylcarbazole produced by certain Ziegler type initiators has been quoted as evidence for a higher measure of stereoregularity.²² The infrared absorption spectrum of benzene-insoluble polymer made in presence of boron trifluoride etherate in methylene dichloride has been found to be identical with that of benzene-soluble polymer obtained by free radical-initiated polymerization.²³ In the absence of any direct evidence for crosslinking or for Friedel-Crafts polymerization which in any case could not account for the insoluble material obtained upon freeradical initiation, its high molecular weight is taken to account for the low solubility of this material.

The results of analysis of the gas isolated from freshly polymerized granules and the apparent good gas permeability of the granule surface indicate that the nitrogen formed on thermal decomposition of the azobisisobutyronitrile does not contribute significantly to the foaming. Only a small proportion of the azobisisobutyronitrile is thought to be dissolved in the monomer, and this is far from sufficient to account for the quantity of gas contained in the granules. All the nitrogen obtainable from the AIBN used under the conditions required for making granules (137 ml./g.) amounts to about twice that contained in granules (density 0.4 g./cc.), but is insufficient to account for the very much lighter polymer (density ${\sim}0.1$ g./cc.) which has been obtained following failure of the dispersing system, nor does the quantity of nitrogen obtainable from the AIBN used for making beads account for their density. It is considered that the foaming is due to vapor formed mainly from water contained in the dispersed monomer spheres during the exothermic phase of the polymerization, since the temperature in the disperse monomer spheres must rise rapidly to well over 100°C.

The high yield of granules obtained with Nonex 64 is remarkable. Lower yields have been reported with Elvanol,⁵ and this has been confirmed during the course of the present work, when it was shown also that the yield is not improved by the use of more initiator. The results point to some involvement of the Elvanol in the polymerization, but no completely satisfactory explanation is available.

The decomposition product of AIBN $(CH_3)_2C(CN)NHCOCH(CH_3)_2$ isolated from the acetone used to extract the polymer granules is no doubt the hydration product of the Schiff's base $(CH_3)_2C(CN)N=C=C(CH_3)_2$, which is a known product of the thermal decomposition of AIBN. No recognizable monomer impurities (e.g., anthracene) have yet been isolated from these extracts, suggesting that they are combined either with the high molecular weight polymer of the granule or bead or with the acetone-soluble polymer of low molecular weight.

There is a strong indication that complete removal of acetone-soluble material from the polyvinylcarbazole granules or beads is desirable if these are to mold well.

If the effect of solvent impregnation is a decrease of the orientation of the polymer molecules during molding, which may explain its beneficial effect upon the molding properties, a more refined interpretation is needed to account for the wide differences in efficacy of various polymer solvents, e.g., dioxane, pyridine, and benzene, being in varying measure beneficial, whereas others such as dimethylformamide and tetrahydrofuran have little if any good effect. Even more remarkable is the specificity of the solute, acetone being suitable while diethyl ether and methanol are not. Thus the effect of impregnation upon the molding properties appears to depend upon polymer, solvent, and solute. Its relation to the flexibility of the polymer molecule is particularly interesting.

The effect of AIBN upon cohesion during molding is thought to be due to the formation from the AIBN of decomposition products which counteract the orientation of the polymer molecules. There is no indication of crosslinking, both solubility and relative viscosity of the polymer being unaffected by molding in presence of AIBN. Addition of monomer to the impregnation solution containing also AIBN may well improve further cohesion and with it especially the tensile properties of the molding. The negligible effect of AIBN upon the expansion during molding is presumably due to the relatively high permeability of the granule or bead surface to nitrogen, so that the latter has a negligible effect compared with that of solvent and solute.

Control of the impregnation by AIBN-dioxane-acetone solution remains a problem requiring further study and particularly needful in the case of beads for which, especially when their molecular weights are high, this is particularly critical.

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Résumé

La polymérisation de vinyl-carbazol en dispersion aqueuse en présence d'azobisisobutyronitrile fournit suivant le colloïde protecteur utilisé des perles ou des granulés de polyvinyl-carbazol. Ceux-ci nécéssitent une imprégnation par un solvant du polymère et, de préférence, contenant aussi de l'azobisisobutyronitrile avant qu'ils puissent être moulés en panneaux ou en des formes bien déterminées.

Zusammenfassung

Die Polymerisation von Vinylcarbazol in wässriger Dispersion mittels Azobisisobutyronitril kann je nach dem verwendeten Schutzkolloid Polyvinylcarbazolperlen oder -körnchen liefern. Diese bedürfen einer Imprägnierung durch ein Lösungsmittel für das Polymere und womöglich durch Azobisisobutyronitril vor einer Verpressung zu Platten oder einfachen Formen.

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